

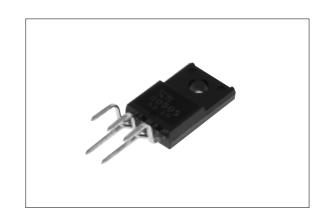
Full-Mold, Separate Excitation Switching Type

■Features

- Compact full-mold package (equivalent to TO220)
- Output current: 3.0A
- High efficiency: 79 to 91%
- Requires only 4 external components
- Phase correction and output voltage adjustment performed internally
- Built-in reference oscillator (60kHz)
- Built-in overcurrent and thermal protection circuits
- Built-in soft start circuit (output ON/OFF control)

■Applications

- Power supplies for telecommunication equipment
- Onboard local power supplies



■Lineup

Part Number	SI-8033S	SI-8050S	SI-8090S	SI-8120S	SI-8150S						
Vo(V) 3.3		5.0	9.0	12.0	15.0						
Io(A)		3.0									

■Absolute Maximum Ratings

Parameter	Symbol	Ratings	Unit		
DC Input Voltage	Vin	43*	V		
Power Dissipation	P _{D1}	18(With infinite heatsink)	W		
i ower bissipation	P _{D2}	1.5(Without heatsink, stand-alone operation)	W		
Junction Temperature	Tj	+125	°C		
Storage Temperature	Tstg	-40 to +125	°C		
SW Terminal Applied Reverse Voltage	Vsw	-1	V		
Thermal Resistance(junction to case)	Rth(j-c)	5.5	°C/W		

^{*}SI-8033S: 35V

■Recommended Operating Conditions

Parameter	Symbol			Unit			
i didilletei	Symbol	SI-8033S	SI-8050S	SI-8090S	SI-8120S	SI-8150S	Offit
DC Input Voltage Range Vin		5.5 to 28	7 to 40	12 to 40	15 to 40	18 to 40	V
Output Current Range	lo			A			
Operating Junction Temperature Range			°C				

■Electrical Characteristics

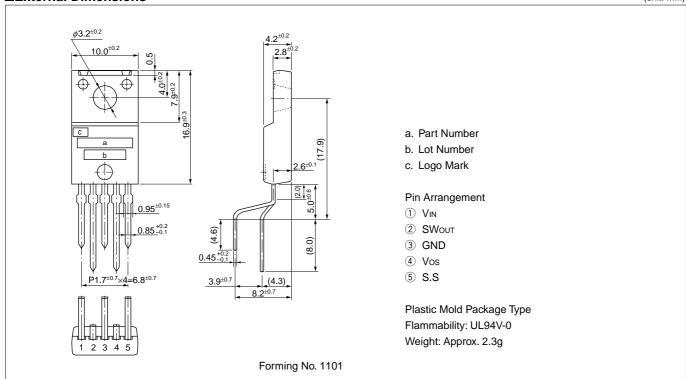
(Ta=25	5°C
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	Parameter		Ratings																
Parame			SI-8033S		SI-8050S			SI-8090S			SI-8120S			SI-8150S			Unit		
			min.	typ.	max.	min.	typ.	max.	min.	typ.	max.	min.	typ.	max.	min.	typ.	max.		
	SI-8000S*1	Vo	3.17	3.30	3.43	4.80	5.00	5.20	8.55	9.00	9.45	11.50	12.00	12.50	14.25	15.00	15.75		
Output	SI-8000SS	VO	3.234	3.30	3.366	4.90	5.00	5.10	8.73	9.00	9.27							V	
voitage	Voltage		Vin=	15V, Io=	1.0A	Vin=	20V, Io=	:1.0A	Vin=	21V, lo=	1.0A	Vin=24V, Io=1.0A Vin=25V, Io=1.0A			1.0A	1			
Efficiency	Efficiency			79			84			88			90			91		%	
Linciency			Vin=	15V, Io=	:1.0A	Vin=	20V, Io=	:1.0A	Vin=	21V, lo=	1.0A	VIN=	24V, lo=	:1.0A	Vin=	25V, lo=	1.0A	70	
Switching Ero	Switching Frequency			60			60			60			60			60		kHz	
Switching Fre			Vin=	15V, Io=	1.0A	Vin=	20V, Io=	:1.0A	Vin=	21V, lo=	1.0A	VIN=	24V, lo=	1.0A	Vin=	25V, lo=	1.0A	NI IZ	
Lino Pogulati	Line Regulation			25	80		40	100		50	120		60	130		60	130	mV	
Line Regulation		Conditions	VIN=8	to 28V, I	n=1.0A	VIN=10 to 30V, Io=1.0A		Vin=15 to 30V, lo=1.0A		Vin=18 to 30V, Io=1.0A			Vin=21 to 30V, Io=1.0A						
Load Pogulat	Load Regulation			10	30		10	40		10	40		10	40		10	40	mV	
Load Negulat			Vin=15	V, Io=0.5	to 1.5A	Vin=20	V, Io=0.5	to 1.5A	Vin=21	V, Io=0.5	to 1.5A	VIN=24V, Io=0.5 to 1.5A VIN=25V, Io=0.5 to 1.5A		to 1.5A] ""v				
Temperature Coefficient	of Output Voltage	ΔVο/ΔΤα		±0.5			±0.5			±1.0			±1.0			±1.0		mV/°C	
Pinnla Paiast	Ripple Rejection	RREJ		45			45			45			45			45		dB	
Kippie Kejeci	1011	Conditions	f=1	00 to 12	0Hz	f=1	00 to 12	0Hz	f=1	00 to 12	.0Hz	f=1	00 to 12	0Hz	f=1	00 to 12	:0Hz	ub	
Overcurrent F	Protection	ls ₁	3.1			3.1			3.1			3.1			3.1			Α	
Starting Current		Conditions	VIN=15V		Vin=20V		Vin=21V		VIN=24V		VIN=25V								

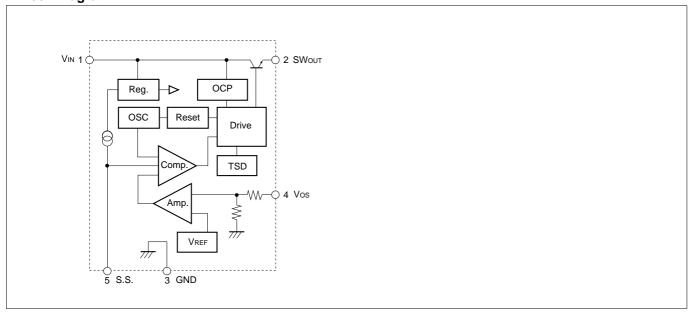
^{*1: &}quot;S" may be indicated to the right of the Sanken logo (except SI-8120S, SI-8150S)



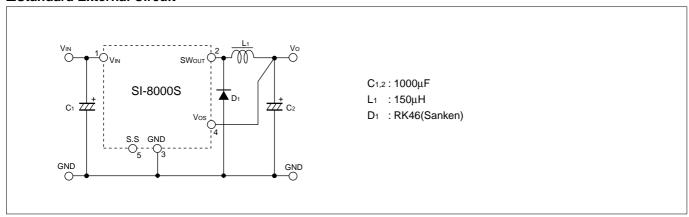
(unit: mm)



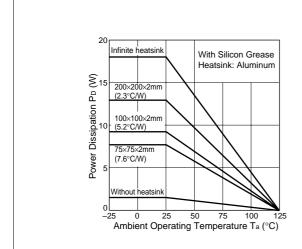
■Block Diagram



■Standard External Circuit



■Ta-PD Characteristics



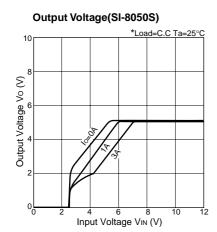
$$P_{D} = V_{O} \bullet I_{O} \; \left(\frac{100}{\eta \chi} - 1 \; \right) - V_{F} \bullet I_{O} \left(1 - \frac{V_{O}}{V_{IN}} \; \right)$$

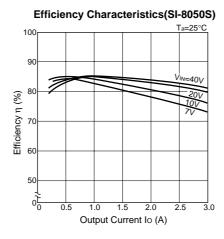
The efficiency depends on the input voltage and the output current. Thus, obtain the value from the efficiency graph on page 75 and substitute the percentage in the formula above.

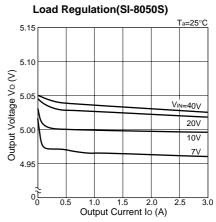
Vo : Output voltage
V_{IN} : Input voltage
Io : Output current
ηx : Efficiency (%)
VF : Diode forward voltage
0.5V(RK46)

Thermal design for D₁ must be considered separately.

■Typical Characteristics

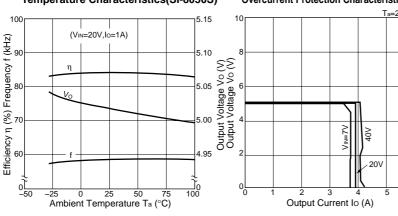


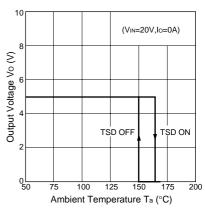




Temperature Characteristics(SI-8050S)

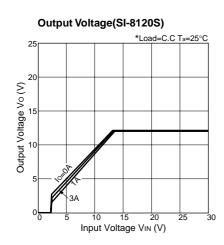
Overcurrent Protection Characteristics(SI-8050S) Thermal Protection Characteristics(SI-8050S)

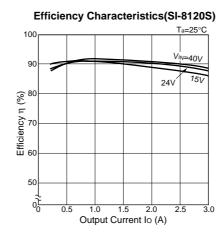


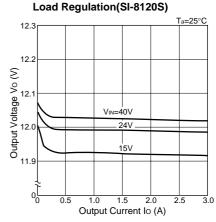


Note on Thermal Protection:

The thermal protection circuit is intended for protection against heat during instantaneous short-circuiting. Its operation is not guaranteed for continuous heating condition such as short-circuiting over extended periods of time.







Application Notes

1. Selecting External Components

(1) Choke coil L₁

To maintain the stable operation of the regulator, choke coil L₁ should be selected appropriately.

When selecting choke coil L₁, consider the following:

 a) Suitable for a switching regulator
 Do not use a coil as a noise filter because it generates excess heat

b) Appropriate inductance

The greater the inductance of the choke coil, the smaller the output ripple voltage. However, the size of the coil increases large as the inductance increases. If the inductance is low, a greater peak current flows to the IC and loss increases. This is not favorable for stable operation.

The standard external circuit shows reference inductance values suitable for stable operation. However, the appropriate inductance may also be calculated as follows:

$$L = \frac{(V_{IN} - V_O) \cdot V_O}{\Delta I L \cdot V_{IN} \cdot f}$$

Where, ΔIL indicates the ripple current of the choke coil that is roughly set as follows:

• If the output current is close to the maximum rating (3 A) of SI-8000S

Ripple current = output current \times 0.2 to 0.3

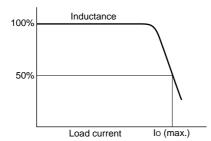
• If the output current is about 1.0A or less
Ripple current = output current × 0.3 to 0.4

c) Satisfying the rated current

The rated current of a choke coil must be greater than the maximum load current. Note that the inductance decreases drastically and an excess current flows if the load current exceeds the rated current of the coil.

d) Good DC current superposition characteristics

The current flowing through a choke coil is a triangular waveform current superimposed on a DC current equal to the load current. The coil inductance decreases as the load current increases. In general, the coil can be used until the inductance drops to 50% of the rated value. Use this as the reference value for selection.



e) Less noise

A drum-type open magnetic core coil can affect peripheral circuits with noise because the flux passes outside the coil. To avoid this problem, use a toroidal, EI, or EE type closed magnetic core coil.

(2) Input capacitor C1

Input capacitor C₁ operates as a bypass capacitor in the input circuit.

When selecting input capacitor C1, consider the following:

- a) The breakdown voltage is higher than the maximum input voltage.
- b) Satisfies the allowable ripple current

Exceeding the ratings of this capacitor or using it without derating may reduce its service life and also cause the regulator to malfunction. Therefore, an input capacitor with a sufficient margin should be selected. With the SI-8000S Series, the effective ripple current Irms flowing to the input capacitor can be calculated approximately as follows:

$$l_{rms} = 1.2 \times \frac{Vo}{V_{IN}} \times lo$$

(3) Output capacitor C2

Output capacitor C_2 operates as a smoothing capacitor for switching output. The output ripple voltage from the regulator is determined by the product of the pulsating current part ΔIL (= C_2 charge-discharge current) of the choke coil current and the equivalent series resistance ESR of the output capacitor C_2 .

$$Vrip=\Delta IL \cdot C2ESR$$

Therefore, a capacitor of low equivalent series resistance ESR should be selected to reduce the output ripple voltage. It is recommended to select a low-impedance capacitor intended for use with switching regulators as C₂.

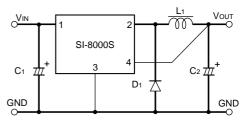
(4) Diode D₁

Use a Schottky barrier diode for D₁. If you use a general rectifier diode or fast recovery diode, the IC may be damaged. (Sanken RK46 recommended)

2. Cautions on Pattern Design

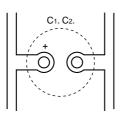
(1) Large current line

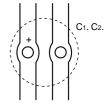
Since a large current flows through the bold lines in the standard external circuit make the pattern as wide and as short as possible.



(2) Input capacitor

Place the input capacitor C_1 and output capacitor C_2 as close to the IC as possible. Since a large current flows through the lead wires of the input and output capacitors to charge and discharge them quickly, minimize the lead wire length. The pattern around the capacitors should also be minimized.





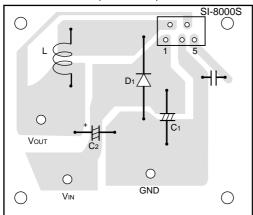
Example of bad pattern

Example of good pattern

(3) Sensing terminal

Output voltage sensing terminal Vos should be connected as close to output capacitor C₂ as possible. If the terminal is far from the capacitor, the decreasing regulation and increasing switching ripple may result in abnormal oscillation.

Example of basic pattern



Top view (with part names)

Applications

1. Soft Start

Connecting a capacitor to terminal no. 5 permits a soft start at power-on. Delay time $T_{\rm d}$ and rise time $T_{\rm s}$ can roughly be calculated as shown below. (However, the values may slightly vary in an actual application.) If the capacitance of C_3 is increased, it takes longer to discharge C_3 after V_{IN} is turned off. Therefore, it is recommended to set the value to $10\mu F$ or less. When not using the soft start function, keep terminal no. 5 open.

$$T_{d=} = \frac{0.7 \times C_3}{20 \times 10^{-6}} \text{ (sec)}$$

$$T_{s=} = \frac{4.845 \times C_3}{V_{IN} \times 20 \times 10^{-6}} \text{ (sec)}$$

$$SI-8000S$$

$$5$$

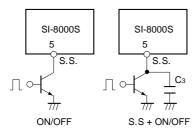
$$S.S.$$

$$C_3$$

$$V_0$$

2. Output ON/OFF control

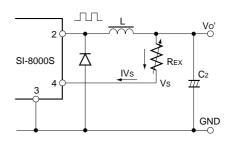
Output can be turned on and off by using the soft start terminals. Set the soft start terminal voltage to VssL (0.2V typ.) or less to stop output. To switch the potential at the soft start terminals, drive the open collector of the transistor. Since the discharge current from C_3 flows to the ON/OFF control transistor, limit the current for protection. The SS terminal is pulled up to the power supply in the IC and no external voltage can be applied.



3. Variable Output Voltage

The output voltage can be increased by connecting a resistor to Vos terminal No. 4. (There is no way of decreasing the voltage)

(1) Variable output voltage with single external resistor



The output voltage adjustment resistance Rex is calculated as follows:

$$Rex = \frac{Vo' - Vs}{IVs}$$

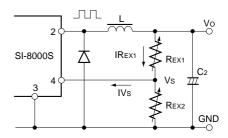
Vs : Output voltage of product Vo' : Adjusted output voltage Ivs : Inflow current to Vs terminal

 * The temperature characteristics of output voltage worsen because the value Rex is not compensated for temperature. The Vs value fluctuates by up to $\pm 20\%$ depending on the IC product. Since the output voltage fluctuates more, a semi-fixed resistor is necessary for accurate output voltage adjustment. If Vs and Rex are constant, the range of output voltage fluctuation can be expressed as follows:

$$\Delta Vo'(\%) = \pm 20 \bullet \frac{Vo'-Vs}{Vo'}$$

ΔVo': Adjusted output voltage

(2) Variable output voltage with two external resistors



The output voltage adjustment resistances Rex1 and Rex2 are calculated as follows:

$$Rex1 = \frac{Vo' - Vs}{S \cdot IVs}$$

$$Rex2 = \frac{Vs}{(S-1) \cdot IVs}$$
S:Stability factor

Bypassing the current to Rex2 improves the temperature characteristics and voltage fluctuation ranges more than the method of (1). Stability factor S indicates the ratio of Rex1 to Vs terminal inflow current. Increasing the S value improves the fluctuations of the temperature characteristics and output voltage. (Usually 5 to 10)

If the Vs and $\mbox{\it Rex}$ values are constant, the output voltage fluctuation range can be calculated as follows:

$$\Delta Vo'(\%) = \frac{\pm 20}{S} \bullet \frac{Vo' - Vs}{Vo'}$$